DESIGN AND CONSTRUCTION OF METALLIC ARTIFICIAL PALM TREE FOR STREET LIGHT AND SURVEILLANCE CAMERA INSTALLATION

1. Buhari ABUBAKAR

Department of Mechanical Engineering, Faculty of Engineering and Technology, Nigerian Defence Academy, Kaduna. buharinmec@gmail.com

2. GARBA, D. K

Department of Mechanical Engineering, Faculty of Engineering and Technology, Nigerian Defence Academy, Kaduna.

- ^{3.} YAKUB Salihu Ochetega Department of Mechanical Engineering, Faculty of Engineering and Technology, Nigerian Defence Academy, Kaduna.
- ABUBAKAR UMAR Nigeria Institute for Oil Palm Research, Benin City, Nigeria

ABSTRACT: The design and construction of a metallic artificial palm tree for street lights and surveillance camera installation is an innovative solution to enhance urban landscapes while incorporating vital functionalities. This work aims to blend seamlessly with the surrounding environment, providing aesthetically pleasing street lighting and discreet surveillance capabilities. The metallic Artificial Palm tree will be engineered using advanced materials and technology, ensuring durability, weather resistance, and high structural integrity. It will mimic the appearance of a natural palm tree, featuring intricate details such as realistic bark texture, lush foliage, and graceful fronds. The design will consider all the environmental factors for smooth construction and installation of the product so as to provide efficient and eco-friendly illumination, promoting safety and enhancing the overall ambiance of the area. By combining the functionality of street lighting and surveillance cameras with the beauty of a natural palm tree, this work aims to create

a harmonious and technologically advanced urban environment. It will enhance the safety, aesthetics, and sustainability of public spaces, fostering a sense of community and well-being.

Keywords: Artificial Palm Tree, SolidWorks, Surveillance Camera, street light

1.0 INTRODUCTION:

Palm trees are not just majestic and iconic; they play a vital role in enhancing the beauty of our surroundings[1]. With their graceful stature and distinct features, palm trees bring a touch of tropical elegance to any landscape, making them an essential element for beautifying our environment. One of the primary reasons palm trees are crucial for enhancing aesthetics is their unique appearance[2]. With their tall trunks and lush, vibrant crowns, palm trees add a sense of grandeur and tranquillity to any setting. Whether they are swaying in the breeze along a beachfront or lining the streets of a city, palm trees create a visual spectacle that captures the imagination and instils a sense of serenity.

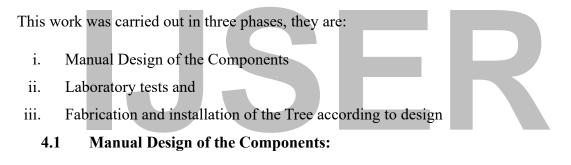
The design and construction of a metallic artificial palm tree for streetlight and surveillance camera installation, carried out in this work, is an innovative and creative approach to blending functionality with aesthetic appeal in urban areas. The artificial palm tree was a specially crafted structure that emulated the natural beauty of palm trees while serving practical purposes. Its primary objective is to provide a discreet and visually pleasing solution for streetlight and surveillance camera placement. By mimicking the appearance of a real palm tree, it seamlessly integrates into the urban landscape, creating an atmosphere that is both inviting and secure. The design process of this Tree involves careful consideration of various factors.

The materials to be selected should be typically sturdy metals, which ensure durability and longevity. The base of the structure should also be designed to be strong and stable, capable of withstanding wind forces and other environmental elements[3]. The streetlights and surveillance cameras, if installed on the artificial Tree, will add an element of functionality to the design. The

streetlights will provide essential illumination, enhancing visibility and safety in the surrounding area, while the cameras will discreetly monitor the surroundings, enhancing security and deterring potential criminal activities.

In this research work, all the components were meticulously constructed and assembled at the Mechanical Engineering Workshop, Nigerian Defence Academy (NDA). The Trunk of the Tree was constructed with precision, replicating the organic patterns and textures found in real palm trees. The branches are strategically positioned to accommodate streetlights and surveillance cameras, ensuring optimal lighting and surveillance coverage.

2.0 MATERIALS AND METHOD



The tree branches, Trunk, and base of the Tree are the most essential constituents of the artificial Palm tree. The well-arranged leaves and branches bring out the aesthetic nature of the Tree. In designing the leaves and stems, For the structural property, each of the leaves/branches is assumed to be a cantilever beam fixed at one end and subjected to shear stress occasioned by the wind loads/pressure of the area [4]. Thus, these loads were evaluated considering the maximum wind speed of Afaka and its environs (where NDA is situated) for a couple of years, as gathered from the Nigerian Metrological Agency (NiMET).

2.1.1 Design theory

Trunk/Pole Design theory

Pole Design Requirements: The trunk design is primarily based on the types of loads acting on the pole. These loads include[5]:

- ✓ Dead Load: These are loads of the branches, the camera, and the wireless router at the top of the pole.
- ✓ Lateral Load: These are loads acting on the Trunk due to wind. This includes wind shear, which may be uniform or linearly acting along the Trunk's height or varying by a cubic polynomial function. To accommodate these loads, the Trunk must have adequate:
- Axial Strength: The critical load capacity of the tower in the axial direction must be greater than the applied axial loads by a safety factor.
- Flexural Strength: The flexural strength of the pole must be greater than the bending strength, i.e., it can sustain the moment generated by the wind force. Also, it can maintain local buckling moments considering the pole's slenderness.

2.1.2 Wind Load calculation: Wind load along the Trunk is applied at extreme wind conditions, which is obtained at the hub height of 10m. At extreme wind conditions in NDA Main Campus, Afaka, the speed is 12 m/s; hence, we selected twice (25 m/sec). This could be converted into pressure according to the following equation[5]:

$$P = \frac{1}{2}\rho V^2 C_d \tag{2.1}$$

Where P = Total pressure of the wind

 $\rho = Air Density = 1.23 \text{ kg/m}^3$

V=25m/sec

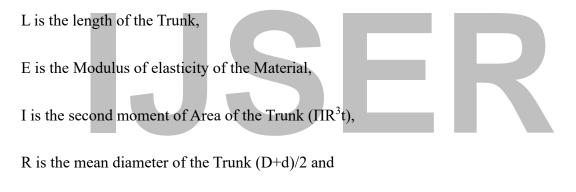
Cd= Drag Coefficient=3.

Accordingly, for Maximum trunk deflection, since we have assumed that the tree trunk behaves as a cantilever beam, the maximum trunk deflection is determined by applying uniform lateral load along its height. So, the maximum deflection δ at the free end is obtained by.

$$\delta \max = \frac{F L^3}{3EI}$$
(2.2)

where;

F is the Force acting uniformly along the height of the tower,

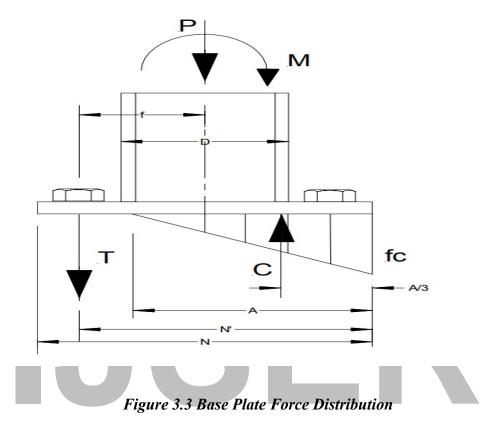


t is the Thickness of the trunk/pole.

The obtained δ must be less than 1% of the total height of the pole [5]. That is $\delta < 0.01$.

2.1.3 Base Plate Design Theory

The base is to be designed to be flexible with the ability to maintain a linear strain distribution, assuming that compression forces are concentrated at the center under the compression flange of the column [6]. Thus;



From Figure 3.3 above, let B = Base plate width

$$T+P = C = \frac{1}{2}(F_c AB)$$
 2.3

$$T = \frac{M - (PD)/2}{F + (\frac{D}{2})}$$
 2.4

$$Fc = \frac{2(T+P)}{A+B}$$
 2.5

2.1.4 Foundation Footing Design Theory

For the foundation design, two loads are to be considered[7]. They are:

- i. Dead load due to the overall weight of the Tree
- ii. Wind loads due to the wind speed of the area

The dead load is the summation of load due to the branches, the Trunk, the base plate, and the concrete base. Its expression is as follows.

For Dead Load,

Load $P_d = \Sigma$ Weight of the component multiplied by acceleration due to gravity

Hence, the summation of the weight in (Kg) is

i.	Weight of the branches W _b (Kg)
ii.	Weight of the Camera Wc
iii.	Weight of the Palm Nut Wp
iv.	Weight of the Street light Ws
v.	Weight of the Trunck Wt

vi. Weight of the Base Plate Wbp

Therefore, load
$$P_d = (W_p + W_c + W_s + W_t + W_{bp}) \ge 9.81 \ge 9.81 \ge W_d$$
 (2.6)

Accordingly, for wind load, applying equation 2.1, Wind Load Pw is given by

$$P_{\rm w} = \frac{1}{2} \rho V^2 C_{\rm d} A \tag{2.7}$$

Hence, the overall load P is given by $P_d + P_w$

$$P = 9.81 \Sigma W_d + \frac{1}{2} \rho V^2 C_d A$$
(2.8)

Therefore, SBC is defined as P/A

Where SBC is the Soil Bearing Capacity of the site

P is the overall load acting on the foundation and

A is the area of foundation

3.0 RESULT AND DISCUSSION

The overall result involves all the design calculations, as well as the stages carried out in the construction and installation of the components.

3.1 Soil Bearing capacity Test for foundation design

A soil sample of the site was obtained for the design of the foundation footing of the Artificial Palm tree. This is to determine its soil-bearing capacity and design the area for the foundation casting[8]. The test was conducted using a Direct Shear Box machine, and the results were obtained using the Terzerghi Principle[9], as presented below.



(a)

(b)

Plate 3.1 a and b Soil Bearing Capacity Apparatus

Accordingly, the test results obtained are presented below:

- i. Mold Dimension = 0.06m by 0.06m by 0.025
- ii. Cross-Sectional Area= 0.0036 m^2
- iii. The volume of the Mold is = 0.00009 m^3

- iv. Force (KN) = (9.81*NL)/1000
- v. Normal Stress = Force/ Cross-sectional area
- vi. Shear Stress = [(Dial gauge reading) x (Machine Calibration factor)] ÷ (Mold Crosssectional area)
- vii. Machine Calibration factor = **0.0043**
- viii. Unit weight of the soil $(V) = 18.92 \text{KN/m}^3$ and
- ix. Dept of the foundation $(D_f) = 2m$

Normal Stress Normal load (kg) Dial gauge Shear Test Force (KN) Stress (KN/m^2) (KN/m^2) No. reading (KN) 27.25 1 10 31 0.0981 37.03 2 20 37 0.1962 54.50 44.19 3 30 43 0.2943 81.75 51.36

Table 3.1 Test result from Direct Shear box machine

From the above table, a graph of Shear stress against Normal stress was plotted on the same scale as shown below to get Apparent cohesion (C) and Friction Angle (\emptyset).

C is the point at which the graph cut the Y-axis, while \emptyset is the angle at which the graph made with the X-axis and is used to trace the Terzaghi factors from the chart shown below:

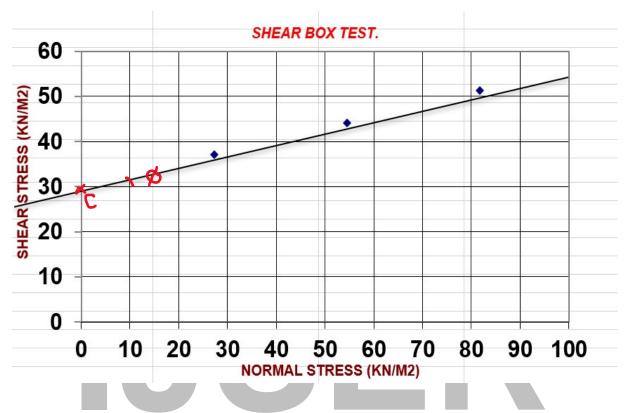


Figure 3.2 Graph of Shear Stress against Normal Stress

¢'	N.	Na	Ny	φ'	N _c	N _a	Ny
0	5.70	1.00	0.00	26	27.085	14.210	9.84
1	6.00	1.10	0.01	27	29.236	15,896	11.60
2	6.30	1.22	0.04	28	31.612	17.808	13.70
3	6.62	1.35	0.06	29	34.242	19.981	16.18
4	6.97	1.49	0.10	30	37.162	22.456	19.13
5	7.34	1.64	0.14	31	40.411	25.282	22.65
6	7.73	1.81	0.20	32	44.036	28.517	26.87
7	8.15	2.00	0.27	33	48.090	32.230	31.94
8	8.60	2.21	0.35	34	52.637	36.504	38.04
9	9.09	2.44	0.44	35	57.754	41.440	45.41
10	9.60	2.69	0.56	36	63.528	47.156	54.36
11	10.16	2.98	0.69	37	70.067	53.799	65.27
12	10.76	3.29	0.85	38	77.495	61.546	78.61
13	11.41	3.63	1.04	39	85.966	70.614	95.03
14	12.11	4.02	1.26	40	95.663	81.271	115.31
15	12.86	4.45	1.52	41	106.807	93.846	140.51
16	13.68	4.92	1.82	42	119.669	108.750	171.99
17	14.56	5.45	2.18	43	134.580	126.498	211.56
18	15.52	6.04	2.59	44	151.950	147.736	261.60
19	16.56	6.70	3.07	45	172.285	173.285	325.34
20	17.69	7.44	3.64	46	196.219	204.191	407.11
21	18.92	8.26	4.31	47	224.549	241.800	512.84
22	20.27	9.19	5.09	48	258.285	287.855	650.67
23	21.75	10.23	6.00	49	298.718	344.636	831.99
24	23.36	11.40	7.08	50	347.509	415.146	1072.80
25	25.13	12.72	8.34			1	

Plate 3.1 Terzaghi's Bearing Capacity Factors

From the graph, C is approximately 29 while \emptyset is around 15 degrees, and the Terzaghi factors Nc, Nq, and N γ are as shown in the table below[10]:

С	Y	Ø	Df	Nc	Nq	Νγ	В	F.S
29	18.92	15	2	12.86	4.45	1.52	1	3

 Table 3.2 Terzaghi's Bearing Capacity Factors

Applying the Terzaghi equation for square footing[11],

 $Q(ult) = 1.3C Nc + VD_f Nq + 0.4VBN\gamma$ (4.1) Substituting the values above, Q(ult) = 664.71336 $Q(safe) = Q(ult)/FS = 664.71336/3 = 221.51 KN/m^2$

We use 220 KN/m²

3.2 Design Calculations for the Tree Components

Below are the design calculations that will guide in the construction of the Tree

Data

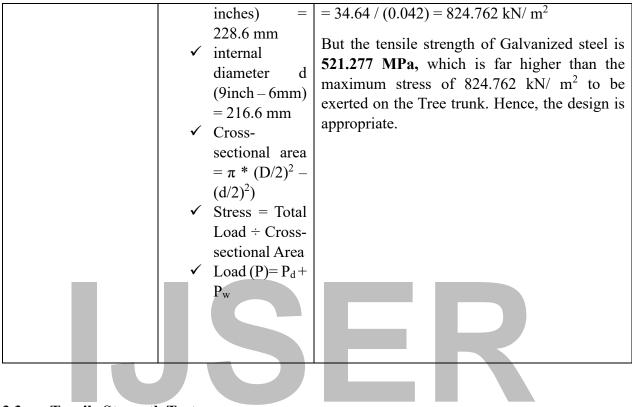
- i. Maximum wind speed for Afaka General Area in the last ten years (m/s) = 12
- ii. Adopted wind speed (m/s) = 25
- iii. Length of Tree (m) = 10
- iv. Inner radius of tree trunk (m) = 0.1083m
- v. The external radius of tree trunk (m)= 0.1143m
- vi. Branch length (m) = 2 each
- vii. Branch weight (kg) = 6.5 each
- viii. Camera weight (kg) = 7.5

- ix. Palm nut weight (kg) = 5 each
- x. Weight of Trunk (kg) = 450
- xi. Weight of base plate (kg) = 38
- xii. Adopted wind speed (m/s) = 25
- xiii. Density of air $(kg/m^3) = 1.225$
- xiv. Drag coefficient $C_d = 3$
- xv. Length of Tree (m) = 10
- xvi. Inner radius of tree trunk (m) = 0.1083m
- xvii. The external radius of tree trunk (m)=0.1143m
- xviii. Soil Bearing capacity SBC $(KN/m^2) = 220$
 - xix. Area of engagement $A = \pi r^2 = 12.568 \text{ m}^2$
 - xx. Dead Load $P_d = 9.81 \Sigma W_d = 588.5 \ge 9.81 = 5,773.185 N$
 - xxi. Live Load $P_w = \frac{1}{2} \rho V^2 C_d A = 28,867.125 N$
- xxii. Load P = 5,773.185 + 28,867.125 = 34,640.31 N = 34.64 kN

Considering the data above, the components of the Tree will be designed to withstand the load and pressure. Thus;

Component	Formulas	Design
Foundation footing	Fr square footing,	From the relation SBC = Load/ Area
(Concrete)	\checkmark Area = L ²	Therefore,
	$\checkmark \text{Load } (P) = P_d + P_w$	Area = Load/ SBC
	\checkmark SBC = Load/	= 34.64 /220 = 0.1574545
	Area ✓ Safety factor	Hence, length $L = sqr(0.1574545)$
	SF = 2	= 0.396
		Applying S $F = 2$,

		L= 0.396 X 2
		L = 0.390 A 2
		= 0.7936
		We select 1m
Pull down bolt (Y32 steel rod selected)		1. Bolt Size: Considering the load of 34.64 kN, the minimum bolt size would be an M20 bolt. We select M32 bolts with a diameter of 32mm, which provides sufficient strength to handle the load.
	JS	 Anchoring Depth: For a 2-meter depth foundation, anchoring the bolt at least 1.5 times the depth is recommended. So, we select an anchoring depth of 3 meters. Thread Design: we use a coarse thread pitch for the bolt, such as 2.5mm or 3mm, to ensure a secure grip and a minimum engagement length of at least five times the bolt diameter, which in this case would be 100mm.
		4. Nut and Washer: We use an M32 nut and a hardened washer to match the bolt size and material. A grade 8 nut and a hardened steel washer were selected for this application.
Base plate	For square base plate, \checkmark Area = L ²	From this relation, Maximum stress = Total load ÷ area
(Iron manganese Alloy selected)	$\checkmark \text{Area} = L$ $\checkmark L = 0.5 \text{m}$	Therefore,
	✓ Load (P)= P_d	$= 34.64 / (0.5)^2 = 138.56 \text{ kN} / \text{m}^2$
	 + P_w ✓ Maximum stress = total load ÷ area 	However, the tensile strength of iron manganese alloy is 350 MPa , which is far higher than the maximum stress of 138.56 kN/ m^2 to be applied on the base plate. Hence, the design is appropriate.
Trunk design	For a trunk of 10m	From this relation, Maximum stress = Total load
(Galvanized iron	high,	÷ Cross-sectional area
round pipe selected)	✓ external diameter D (9	Therefore,



3.3 Tensile Strength Test

A laboratory test for the tensile strength of the selected samples was also carried out[12]. This is to reconfirm that the materials purchased for the construction are in tandem with the result obtained from the design. Hence, the test is presented below:

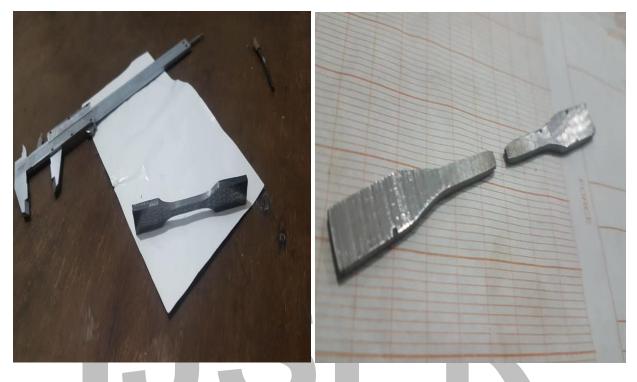


Plate 4.6 Galvanizes steel before the tensile test

Plate 4.7 Galvanizes steel after tensile test

Result data

Total length (Lt) = 100mm

Original gauge length (Lo) = 25mm

Final gauge length (L) = 29mm

Original width (Wo) = 4.7mm

Final width (W) = 3.7mm

Original thickness (to) = 4mm

Final thickness (t) = 3.2mm

Load at failure (Pmax) = 9800 N

Ultimate Tensile Strength is given by the equation $\sigma \max = \frac{P \max}{Ao}$ (2.9)

But Ao = Wo x to $= 18.8 \text{ mm}^2$

Hence $\sigma \max = \frac{9800}{18.8} = 521.277 \text{ MPa}$

= 5.21 X 10⁸ Pa

Accordingly, Axial Strain is given by $\mathcal{E} = \frac{\Delta L}{Lo}$ (2.10)

(2.11)

Hence $\xi = \frac{4}{25} = 0.16$

Meanwhile, Elastic Modulus E $=\frac{\sigma}{\epsilon}$

Hence E $= \frac{\sigma}{\epsilon} = 5.21 \text{ X } 10^8 / 0.16$

= 3.26 x 10⁹ Pa (Modulus of Elasticity of the Material)

3.4 Material selection based on designed results[13][14][15]

Table 2.0	Material	Selection	Table
1 abic 2.0	1 autian		

s/n	Tree	Propo	sed Materials	Selected material	Reason of	Yield
	component				selection	Strenght
1	Leaves	i.	Mild steel	0.7mm	Ductility,	250-350 MPa
		ii.	Galvanize	Mild steel	availability,	
			steel	sheet	machinability,	
		iii.	Stainless		and cost[16]	
			steel			
		iv.	Fiber			
			material			
2	Petiole	i.	Y16 mild	Y16 mild	Versatility,	250-350 MPa
	(stem)		steel rod	steel rod	weldability,	
		ii.	16mm		availability,	
			galvanized		and cost[17]	
			round pipe			
		iii.	Stainless			
			steel round			
			pipe			
				<u> </u>		200 400 1 55
3	Trunk	i.	Mild steel	Galvanize	Strength,	200-400 MPa
			pipe	iron pipe	corrosion	
		ii.	Stainless		resistance,	
			steel pipe		and cost[18]	

			Galvanize			
		111.				
			iron pipe			
		iv.	Wood			
		v.	Concrete			
4	Trunk	i.	Mild steel	Aluminum	Heat	137-483Mpa
	bottom		sheet	sheet	resistance and	
	(D 1 (ii.	Aluminum		corrosion	
	(Bucket-		sheet		resistance[19]	
	like)	iii.	Stainless			
			steel sheet			
5	Trunk base	i.	Mild Steel	Iron	Strength,	200- 500Mpa
	(Daga Dlata)	ii.	Iron	manganese	Toughness,	Ĩ
	(Base Plate)	ii.	Iron manganese	manganese alloy	Toughness, corrosion	1
	(Base Plate)	ii.		•	-	
	(Base Plate)	ii. iii.	manganese	•	corrosion	
	(Base Plate)		manganese alloy	•	corrosion resistance,	
	(Base Plate)		manganese alloy Galvanize	•	corrosion resistance,	
	(Base Plate)		manganese alloy Galvanize	•	corrosion resistance,	
	(Base Plate)		manganese alloy Galvanize	•	corrosion resistance,	
	(Base Plate)		manganese alloy Galvanize	•	corrosion resistance,	

3.5 Construction of the Palm Tree

The step-by-step procedures performed in the construction of the artificial palm trees are itemized below:

Step I: Leaves and Branch Construction

- i. 4X8 feet length of 0.7mm steel sheet was obtained
- ii. A natural palm tree leave was equally obtained from a life palm tree
- iii. The raw leaves were placed on top of the sheet and traced to bring out their shape
- iv. A cutting scissors was used to cut the traced pattern of the leaves
- v. A mold was also used to create the stem pattern in the middle of the sheet
- vi. A flat metal bar was used on each leave to produce the V-shape on the leaves

- vii. A Y16mm steel rod was welded at the center of the sheet/leaves to form the stem
- viii. The worked sheet was bent to create an arc of a leaf shape.
 - ix. A quarter rod was welded at both sides of the leaves for brazing and separation purposes
 - x. A body filler was applied to the leaves sheet to give it a better shape and address possible corrosion
 - xi. The whole leaves and branch were painted green color, as shown in the figure below:



Plate 3.5 Artificial palm leaves

Step II: Trunk Construction

- A 9-inch by 6mm thick galvanized iron round pipe was obtained in two segments (6m and 5m long)
- ii. 1m length was removed from the 5m length pipe using cutting stone to remain only 4m length
- iii. The 9inch diameter of the 1m pipe was trimmed down to $8^3/_4$ inch slim pipe to be used as an internal socket connecting the two pipes
- iv. The slim pipe was inserted into the two pipes midway, forming a socket joint of a total length of 10m
- v. A plumb was used to align the pipe before final welding
- vi. The pipe was then welded at the joint of the two end pipes and equally rivet welded at various positions, as shown in the figures below:



(a)



Step III: Base plate and foundation bolt Construction

- i. 20 inches by 20mm Iron Manganese Alloy was obtained as a base plate
- ii. Four holes of 35mm diameter were created using gas cutting machine at an interval of 200mm from the midpoint of the plate
- iii. Four pieces of Y32mm by 6 feet steel rod were also obtained
- iv. The rods were threaded to M32 at the top end of the rods for about 4inch (102mm) length
- v. All four rods were bent at the other end to about 6-inch (152mm) length
- vi. Six rings were also constructed with Y12mm steel rod and welded to the Y32mm at equal interval
- vii. Another Y12mm steel rod was used to build a foundation basket of 1square meter with the aid of a binding wire
- viii. A foundation base plate and anchor bolt were built as shown in the figure below:



Step IV: Construction of Foundation

- i. One square meter by 2m depth foundation hole was dogged
- ii. The base of the hole was blended with a concrete mixture to about 12 inches (305mm)
- iii. The already constructed basket was placed on top of the blending.
- iv. The constructed foundation bolt is also placed at the center of the basket and tied with binding wire.
- v. Several sizeable stone rocks were inserted into the hole, and a concrete mixture was added to a reasonable level.
- vi. Plumb was used to adjust the position of the foundation bolt to align vertically.
- vii. Further concrete mixture was finally put up to the surface level. Figure 4.22 shows the constructed foundation base.



Plate 3.7 Hold down bolt and Basket Assembly and Casting.



Plate 3.8 Foundation casting

3.6.5 Palm Tree and surveillance system assembly

To assembly the components of the palm tree, the steps are as follows:

Step I

- i. With the help of spirit bob and square plumbs, the base plate was welded to the end of the round pipe.
- ii. Eight brazing plates were also welded to the pipe and the base plate at equidistance to each other.
- iii. The pipe was painted in two segments (Green on the upper side and dark ash on the lower side)
- iv. With the aid of a motorized forklift, the pipe was raised and fixed to the foundation bolt.
- v. A Plumb was used again to align the pipe vertically before tightening the foundation bolts.
- vi. A scaffold was assembled around the erected pipe for easy access to the top of the pipe.
- vii. With the help of a rope, the leaves were taken up and assembled, as shown in the figure below:



Plate 3.9b Alignment of the tree trunk



Plate 3.9c Assembling of leaves



Plate 3.9d Assembled Palm tree

4.0 CONCLUSION

This novel work designed and constructed an artificial Palm Tree. In line with its objectives. The successful construction of an artificial palm tree has proven to be a remarkable achievement in combining functionality and aesthetics. The designed results of this palm tree have surpassed expectations, offering a multitude of benefits to the environment, community, and overall visual appeal. By seamlessly integrating this lifelike palm tree into its surroundings, we have created a harmonious and natural landscape that captivates the imagination. The realistic design, down to the finest details, ensures that the artificial palm tree blends in seamlessly, maintaining the beauty and integrity of the environment. Not only does this artificial palm tree provide a stunning visual element, but it also serves a practical purpose. The ability to incorporate energy-efficient LED lights within the Tree's structure will ensure efficient and eco-friendly illumination of public spaces. This innovative feature not only enhances safety but also contributes to reducing energy consumption and operational costs.

Additionally, the discreet placement of surveillance cameras within the artificial palm tree enhances security measures without compromising the aesthetic appeal. This strategic positioning helps create a safer environment, promoting peace of mind for residents and visitors alike. Furthermore, the successful construction of this artificial Tree showcases our commitment to sustainability. With durable and weather-resistant materials, this Tree requires minimal maintenance, reducing expenses and conserving resources in the long run. By opting for an artificial palm tree instead of real ones, we are also preserving natural habitats and ecosystems.

In conclusion, the results of this artificial palm tree design have demonstrated the incredible potential for sustainably combining functionality and aesthetics. This creation highlights the importance of innovation in enhancing our environment, community, and overall visual appeal. Through this achievement, we have not only beautified our surroundings but also contributed to creating a greener and more sustainable future.

References

- K. M. Ibrahim, "The Role of Date Palm Tree in Improvement of the Environment," *Coll. Sci. Al-Nahrain Univ. Iraq*, pp. 1–4, 2010.
- [2] E. Davison and J. Begeman, "Arizona Landscape Palms," p. 16, 2000.
- [3] D. Saba, "Investigating the durability of structures," pp. 93–96, 2018.
- Z. Shahbazi, A. Kaminski, and L. Evans, "Mechanical Stress Analysis of Tree Branches," *Am. J. Mech. Eng.*, vol. 3, no. 2, pp. 32–40, 2015, doi: 10.12691/ajme-3-2-1.
- [5] A. Rafai, N. Rahman, and S. Atif Iqrar, "Optimal Design of Pole for Solar Wind Hybrid Energy System," *Int. J. Eng. Inf. Syst.*, vol. 2017, no. 4, pp. 66–79, 2017, [Online]. Available: www.ijeais.org
- [6] D. Horn, *Technical Manual 1: Design of Monopole Bases*. 2011. [Online]. Available: www.towernx.com
- [7] D. P. C. W. A. Kitch and M. R. Yeung, *Foundation Design, Principles and practices*, vol. 52, no. 204. 2011. doi: 10.51952/9781447343264.ch004.
- [8] L. Hashemian, N. Tavafzadeh, and A. Bayat, "Evaluation of pavement load bearing capacity comprised of insulation layers during thaw season," *Bear. Capacit. Roads, Railw. Airfields*, no. November 2019, pp. 833–837, 2017, doi: 10.1201/9781315100333-111.
- [9] H. H. Vaziri and H. A. Christian, "Application of Terzaghi's consolidation theory to nearly saturated soils," *Can. Geotech. J.*, vol. 31, no. 2, pp. 311–317, 1994, doi: 10.1139/t94-037.
- [10] "Terzaghi's Bearing Capacity Square Foundation," *Power Electron. Appl. to Ind. Syst. Transp.*, vol. 2, pp. 255–263, 2016, doi: 10.1016/b978-1-78548-033-1.50008-6.
- [11] hamidomer, "Terzaghi's Bearing Capacity Equations," pp. 1–5, 2009.
- [12] O. Mohammed and E. Suleiman, "Laboratory experiments tensile testing," no. July, 2019.
- [13] R. LeSar, Materials selection and design. 2013. doi: 10.1017/cbo9781139033398.015.
- [14] I. Mazínová and P. Florian, "Materials selection in mechanical design," *Lect. Notes Mech.*

Eng., vol. 16, pp. 145–153, 2014, doi: 10.1007/978-3-319-05203-8_21.

- [15] G. T. Murray, Handbook of Materials Selection for Engineering Applications. 1997. doi: 10.1201/9781482292237.
- [16] M. Engineering, "PROPERTIES EVALUATION OF MILD STEEL, MEDIUM CARBON STEEL AND HIGH CARBON".
- [17] M. N. Sultana, F. Hasan, and M. Islam, "Analysis of Mechanical Properties of mild steel Applying Various Heat treatment Analysis of Mechanical Properties of mild steel Applying Various Heat treatment," no. July, 2020.
- [18] Z. Ghasemivinche and A. Z. Hamadani, "Predicting Mechanical Properties of Galvanized Steels : Data Mining Approach," no. 7, 2017.
- [19] A. Z. H. BIN RAMLI, "EFFECT OF HEAT TREATMENT ON THE CORROSION RESISTANCE OF ALUMINIUM ALLOYS," *Theor. Appl. Genet.*, vol. 7, no. 2, pp. 1–7, 2010, [Online]. Available: http://dx.doi.org/10.1016/j.tplants.2011.03.004%0Ahttp://dx.doi.org/10.1016/j.pbi.2010.0 1.004%0Ahttp://www.biomedcentral.com/1471-2156/12/42%0Ahttp://dx.doi.org/10.1016/j.biotechadv.2009.11.005%0Ahttp://www.scien cemag.org/content/323/5911/240.short%0Apape
- [20] V. Varadaraajan, "Development of a novel iron-manganese alloy and its application," no. February 2015, 2015.